

# Separation of Losses of an Induction Motor

## Objective:

To separate the various losses occurring in an induction motor.

## Theory:

Apart from the calculable  $I^2R$  loss, the losses occurring in an induction motor include the following:

$P_b$  = brush friction loss

$P_e$  = eddy current loss in iron

$P_f$  = mechanical losses in windage and bearing friction

$P_h$  = hysteresis loss

$P_p$  = pulsation loss

The suffices 1 and 2 refer to stator & rotor quantities respectively. At standstill the rotor core loss is  $p_{e2} + p_{h2}$ , when the rotor is open-circuited. At a slip  $s$ , this loss becomes  $s^2 p_{e2} + s p_{h2}$ .

The pulsation loss is a high-frequency tooth loss in stator & rotor, produced by variations of gap reluctance as the tooth tips pass each other.

The friction loss can be separated by the no-load test.

## Procedure:

The following procedure separates all losses for the slip-ring motor:

### **No-load Test**

1. Measure the power supplied to the stator at normal voltage & at rest. The stator input corrected for  $I^2R$  loss is the iron losses  $P1 = p_{e1} + p_{h1} + p_{e2} + p_{h2}$
2. Measure the power supplied to the stator at normal voltage and frequency with the rotor short-circuited and running on no-load. The corrected stator input is  $P2 = p_{e1} + p_{h1} + p_p + p_f + p_b$ .

The rotor eddy current loss is small since it is proportional to  $s$ .  $p_{h2}$  is also supplied by the stator, but practically the whole of it is returned as a driving torque, partly providing for  $(p_f + p_b)$

3. With machine running as in (2), the rotor circuit is suddenly opened and the stator input measured. The stator input falls to  $P4 = p_{e1} + p_{h1} + p_{h2}$ .

### **Transformation Ratio test**

4. Apply a voltage to the rotor such that the stator voltage is  $(V1+v1)/2$  on open circuit, and the mutual flux is normal where  $V1$  is the normal stator applied voltage and  $v1$  is the measured stator voltage when the normal voltage  $V2$  is applied to the rotor.

Measure the rotor input when running on no-load with the stator short-circuited. This corresponds to the condition of (2), except that the functions of the rotor & stator are reversed. The corrected rotor power input is  $P_5 = p_{e2} + p_{h2} + p_p + p_f + p_b$ .

5. With the machine running as in (4), the stator is suddenly open-circuited and the rotor power input falls to  $P_6 = p_{e2} + p_{h2} + p_{h1}$ . This test corresponds to Test3  
The mechanical losses  $P_7 (= p_f + p_b )$  are evaluated by the no-load test

### Locked Rotor Test

7. Measure the power supplied to the stator at reduced voltage and full-load stator current, with the rotor short-circuited & locked. This test gives the  $I^2R$  loss of the machine.

### Observations:

**Induction Motor Specifications: 110 V, 36A, 3-phase, 50Hz, Y-connected, 1440 RPM**

#### 1. Transformation Ratio test

Rotor voltage =  
Stator voltage =  
Therefore, Turns Ratio =

#### 2. No-load test

**Wattmeter constant**  
**C.T Ratio =**

No:	V(L-L) (Volts)	W1 (Watts)	W2 (Watts)	W1+W2 (Watts)	Power (Watts)	$V(L-L)^2$ (Volts) <sup>2</sup>

#### 3. Locked Rotor test

**Wattmeter constant**  
**C.T Ratio =**

No:	V(L-L) (Volts)	I (amps)	W1 (Watts)	W2 (Watts)	W1+W2 (Watts)	Corrected power (Watts)

Stator resistance per phase =

### Calculations:

#### From no-load test

$P_7 = p_f + p_b$  Watts  
 $p_{e1} = P_1 - P_6$  Watts  
 $p_{e2} = \dots$  Watts  
 $p_{h1} = P + (P_2 - P_5 - P_1) / 2$  Watts

$$p_{h2} = P_4 + (P_6 - P_1 - P_2) / 2 \text{ Watts}$$

$$P_p = ((P_5 + P_2 - P_1) / 2) - P_7 \text{ Watts}$$

Assuming  $p_b = p_f = P_7 \text{ Watts}$

### From locked rotor test

$$I_{f,1} = \text{-- amps}$$

$$V_1 = \text{Reduced Voltage, Volts}$$

$$I_{SC1} = \text{-- amps}$$

$$P_{SC1} = \text{-- Watts}$$

Corresponding Values for normal voltage V will be:

$$I_{SC} = V I_{SC1} / V_1 \text{ amps}$$

$$P_{SC} = P_{SC1} (V / V_1)^2 \text{ Watts}$$

$$\text{Stator } I^2R \text{ loss} = 3(I_{SC})^2 R \text{ Watts}$$

$$\text{Rotor } I^2R \text{ loss} = P_{SC} - 3(I_{SC})^2 R \text{ Watts}$$

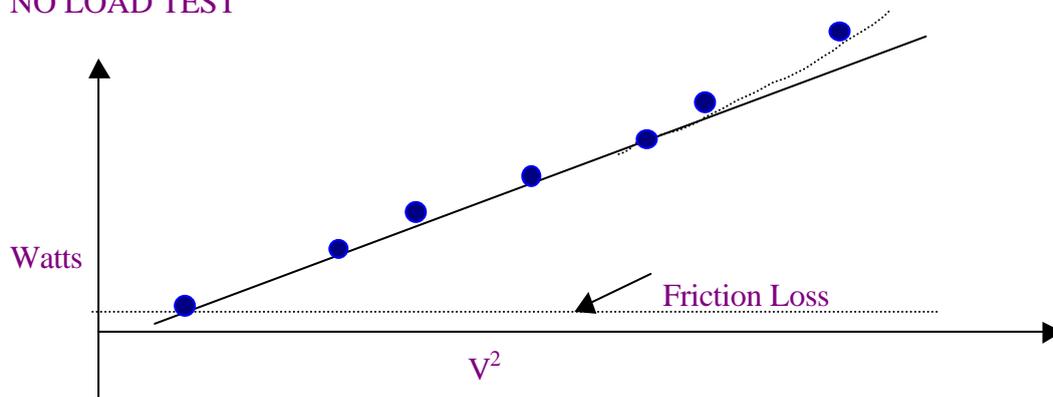
### Results:

1. Eddy loss in stator =-- Watts
2. Eddy loss in rotor =-- Watts
3. Hysteresis loss in stator =-- Watts
4. Hysteresis loss in rotor =-- Watts
5. Pulsation loss =-- Watts
6. Friction + Windage loss =-- Watts

### Discussion:

1. The brush friction loss cannot be measured if there is no internal short-circuiting device. In that case, assume  $p_b = 0$ .
2. The rotor eddy current loss is very small, because it is proportional to  $(\text{slip})^2$  and the slip itself is very small.
3. To get accurate results, the voltage should be maintained constant

### NO LOAD TEST



# LOCKED ROTOR TEST

